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Demand response within the energy-for-water-nexus - A review

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Abstract: A promising tool to achieve more flexibility within power systems is demand re-sponse (DR). End-users in many strands of industry have been subject to research up to now regarding the opportunities for implementing DR programmes. One sector that has received little attention from the literature so far, is wastewater treatment. However, case studies indicate that the potential for wastewater treatment plants to provide DR services might be significant. This review presents and categorises recent modelling approaches for industrial demand response as well as for the wastewater treatment plant operation. Furthermore, the main sources of flexibility from wastewater treatment plants are presented: a potential for variable electricity use in aeration, the time-shifting operation of pumps, the exploitation of built-in redundancy in the system and flexibility in the sludge processing. Although case studies con-note the potential for DR from individual WWTPs, no study acknowledges the endogeneity of energy prices which arises from a large-scale utilisation of DR. Therefore, an integrated energy systems approach is required to quantify system and market effects effectively.

Keyword(s): Energy-water nexus, demand response, wastewater treatment, flexibility, energy system, modelling

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1 Introduction

Energy and water systems are intertwined in many areas. These linkages, where one of these resources is necessary to provide the other, are referred to as the energy-water-nexus. Growing water scarcity and increasing energy demands can create challenges that will require a trade-off. Research on the energy-water nexus has increased in recent years, with the objective of identifying efficient solutions which minimise resource intensity. Within the energy-water nexus, one can distinguish between two subfields: water-for-energy and energy-for-water. In the case of the former, research deals with optimisation of water-usage for providing energy directly or indirectly. Meanwhile, energy-for-water focuses on the energy consumption in the water cycle, which includes potable water treatment, water distribution and wastewater treatment.

While the electricity consumption in water treatment and distribution is comparably low, wastewater treatment is an electricity-intensive process, with electricity costs generally being the highest costs in medium and large-scale wastewater treatment plants (WWTP). Depending on treatment level and plant size, estimated electricity costs can range from 2 percent to 60 percent of total operating costs. In countries with well-developed water distribution and treatment systems, the wastewater treatment sector can be a big electricity consumer, accounting for about 3 percent of total electricity consumption of a country per year [Gude, 2015].

Several case studies have found that energy-consuming processes within the WWTP such as pumping or aeration allow for flexible operation (see section 5.2). This potential flexibility in operation, coupled with significant levels of total energy consumption, makes the wastewater treatment sector an interesting potential source of flexibility from a power system perspective. With the increasing power generation capacity from renewable energy sources (RES), energy supply becomes more and more variable. This necessitates more flexible energy demand sources, which can adapt to the variability in supply by providing Demand Response (DR). DR can be defined as "changes in electric use by demand-side resources from their normal consumption patterns in response to changes in the price of electricity, or to incentive payments designed to induce lower electricity use at times of high wholesale market prices or when system reliability is jeopardized." [Lee et al., 2013]. The implementation of DR programmes can help reduce the risk of power outages, postpone capacity investments, improve the reliability of the system and is likely to reduce electricity cost for energy consumers [Kim and Shcherbakova, 2011]. Research has looked at the potential of different industrial processes to provide DR (see section 3 and 4.2), but assessment of the DR potential of the wastewater treatment sector is still limited.

In this paper, we summarise the published literature on different modelling approaches for industrial DR both from a power system perspective and an end-user perspective. We find that there are no models which account for both aspects simultaneously in sufficient detail. We also point out that traditional WWTP modelling does not account for DR so far, although several case studies indicate that there is significant potential for flexibility within WWTP operation. Case studies have analysed the potential for flexibility in wastewater pumping, intermittent aeration, using built-in redundancy for delaying treatment and sludge processing. The purpose of this paper is to demonstrate that the lack of modelling tools in this area leads to an underutilisation of readily available demand flexibility by WWTPs. An integrated energy-water system model which captures these flexibility options in a WWTP process model in connection with the power system in order to fill this gap does not yet exist.

The paper is structured as follows. Section 2 describes the energy-water nexus and outlines water requirements in the energy sector and the energy usage in water services.

We give a definition of DR and outline its potential benefits and challenges in Section 3. Thereafter, section 4 summarises the literature about existing energy models which analyse industrial DR. We distinguish between energy and power system models on the one hand and end-user focused process models on the other hand. In Section 5, we first explain how the WWTP process is traditionally modelled and then go into detail about where the flexibility potentials within the process lie. We discuss the current modelling approaches for industrial DR in section 6 and propose the development of a combined system-process model for the analysis of the DR potential from WWTPs. We conclude that an integrated energy-water system model of the power system and the wastewater treatment system for the analysis of DR from WWTPs would best capture the effects on the power system and the WWTP operation simultaneously.

2 The energy-water nexus

In regions without water shortages, the linkages between water and energy have mostly not been in the focus of research. However, the trade-off between the resources intensifies. On the one hand, electricity supply is water-intensive, because thermal power plants need constant cooling, and hydro power is an important renewable energy source in some countries. On the other hand, water and wastewater treatment becomes more energy-intensive due to advances in technology and stricter water quality standards. The OECD acknowledges that “efficient management of the [land-energy-water] nexus resources needs to take into account the direct and indirect effects of changes in the demand and supply of the various resources on the whole biophysical and economic systems, as this is the only means to avoid negative side effects and to create synergies“ [OECD, 2017].

Against the background of climate change, increasing global energy demand and increasing water scarcity [Rodriguez et al., 2013], research on the energy-water nexus has recently gained more and more interest. The connections between the energy sector and the water sectors have been first recognised in the early 2000’s, for example with a focus on India [Malik, 2002] or California, US [Lofman et al., 2002]. A keyword search for ‘energy-water nexus’ on SCOPUS [SCOPUS, 2019] reveals that the number of publications on the energy-water nexus has increased significantly since then (figure 1).

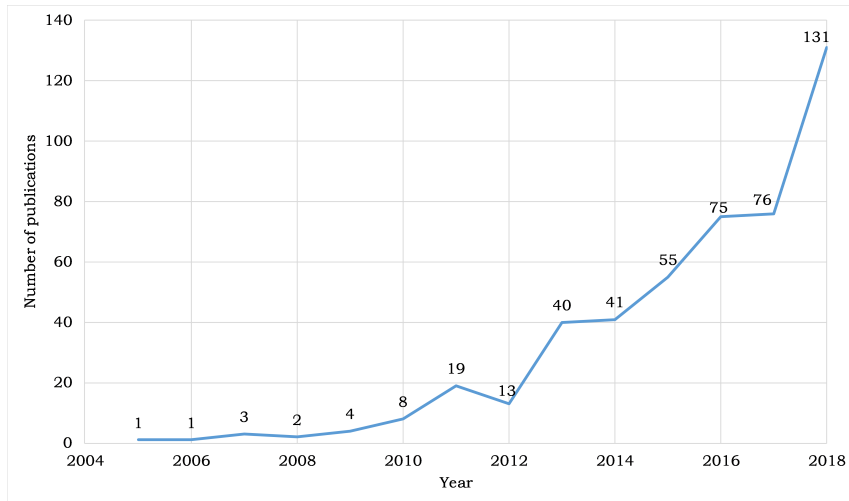


Figure 1: Number of publications on the energy-water nexus per year

In general, the energy-water nexus (sometimes also the energy-water-food nexus or the energy-water-land nexus) refers to all processes which represent linkages between the water system and the energy sector, and the trade-off of both resources. Water is required for energy production (water for energy, see section 2.1), energy is required for water

services (energy for water, see section 2.2), and both resources have close interconnections in production and consumption of products.

Hamiche et al. [2016] further subdivides the energy-water nexus into five different dimensions: environmental, economic, political, social and technological, each of which impose different challenges on water and energy security (see figure 2, based on Hamiche et al. [2016]).

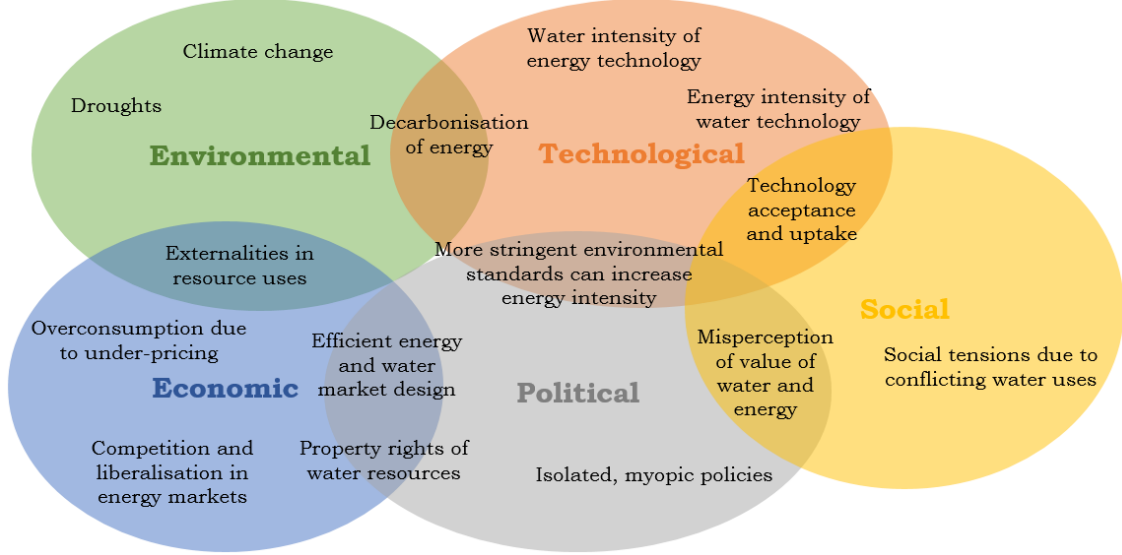


Figure 2: Dimensions of the energy-water nexus and respective challenges (based on Hamiche et al. [2016])

Within the environmental dimension of the energy-water nexus, the main challenge for managing the linkages between energy and water is climate change. Especially in drought-prone regions, climate change intensifies the trade-off between using water for energy generation, human consumption or agriculture. Therefore, analysis often concerns the energy-water-land or the energy-water-food nexus. In the economic dimension, the liberalisation of energy markets also puts pressure on the energy-water nexus. Due to under-pricing, overconsumption is a common phenomenon in both sectors. A major challenge in the political dimension of the energy-water nexus is the political recognition of the energy-water nexus and the replacement of isolated, myopic policies in favour of a joint energy-water strategy. Regarding the social dimension, the conflicting uses of water can give rise to social tensions. It is also a socio-political challenge within the energy-water nexus to correct for a public misperception of the value of water and energy, which can in turn be a reason for overconsumption. Finally, the technological dimension of the energy-water nexus is concerned with the energy intensity of water services and the water intensity of energy services. These are investigated in the following two sections.

2.1 Water for energy

The United Nations [2015] estimate that around 15 percent of global water withdrawals are used for energy generation. However, water withdrawal includes water consumption, losses and recycling back into the water cycle for further usage. While this means that the water withdrawal rate is not necessarily an indicator of water scarcity, water withdrawn for non-consumptive purposes can still impede the alternative use of water in other aspects of the economy at the time of withdrawal. The International Energy Agency [2016] estimates that only about 12 percent of all water withdrawals by the global energy sector are actually consumed, while the majority is recycled. However, water use for energy production is projected to increase within the next decades, due to a continuing increase

in nuclear power generation and biofuel production [International Energy Agency, 2016].

Almost all energy generators require water at some stage of the generation process [Rodriguez et al., 2013]. According to the International Energy Agency [2016], the power generation sector was responsible for about 88 percent of global energy-related water withdrawals in 2014. Thermal power plants require water for cooling purposes. Although the water usage for cooling is mainly not consumptive, it has consequences in terms of water quality (e.g. thermal pollution) and availability for other uses [OECD, 2017]. The share of water withdrawal from fossil fuel power plants in the overall energy sector was about 58 percent in 2014 [International Energy Agency, 2016]. In comparison, wind energy requires virtually no water and solar energy requires only little amounts of water to clean the photovoltaic panels.

Although the International Energy Agency [2016] estimates that only 12 percent of water withdrawal in the energy sector is related to the production of primary energy, it accounts for the majority of water consumption (64 percent). For example, the extraction and refining of fossil fuels such as coal, oil, and shale gas requires large amounts of water. Oil extraction requires water injection into the reservoirs to increase their capacity [OECD, 2017]. Hydraulic fracturing (fracking) which is used in shale gas and oil production, also consumes high quantities of water. Growing crops for biofuel production accounts for 25 percent of global energy-related water consumption [International Energy Agency, 2016]. Water scarcity and water pollution caused by the growing of crops and the production of fuel from these crops poses environmental threats, especially to drought-prone regions. Although biofuel production is projected to grow in China, India and Brazil, production is particularly stagnating in the US and in Europe [The International Energy Agency, 2019].

Power generation in hydro power plants also relies on water to pass through the turbines [OECD, 2017]. Most of the water can be reused without a change of quality or temperature. However, hydro power with reservoir water storage, in contrast to run-of-the-river, can cause water losses due to evaporation. Moreover, hydro power can conflict with other purposes as release schedules do not always match the timing of other water needs such as irrigation [OECD, 2017]. The water consumption of hydropower plants is site-specific and there is no universal measurement methodology yet [International Energy Agency, 2016]. It depends on many different factors such as technology type (reservoir versus run-of-river), reservoir size, climate and demand from other surrounding end-users. Therefore, the International Energy Agency [2016] does not provide an estimate of global water withdrawal and consumption for hydro power.

Finally, water ways like rivers or seas represent routes of transport for primary energy sources such as coal. There is no water withdrawal or consumption involved, but the use for energy transport impedes alternative uses of the water way and causes pollution through the emissions of ships which deteriorates the water quality. Especially in longer periods of hot weather conditions, the consequent water scarcity of rivers can hamper fossil fuel energy generation, when not enough resources can be shipped towards generation facilities.

2.2 Energy for water

It is estimated that 7 to 8 percent of global energy consumption is used to lift groundwater, desalinate sea water and pump and treat both freshwater and wastewater [UNESCO, 2012]. Within each stage of the water cycle, energy is required for various reasons. Most of the energy consumed in fresh water supply and treatment is due to pumping and disinfection. In a conventional water treatment plant with coagulation, flocculation, sedimentation and filtration, the total energy requirement varies between 0.25 and 1 kWh per m^3 of treated freshwater [Gude, 2015]. In general, the treatment of ground water or surface fresh water

is not highly energy-intensive. In contrast, desalination of sea water or brackish water, which is sometimes necessary in dry regions with close proximity to the sea, is very energy-intensive. The process consumes up to 20 kWh per m^3 of treated water [Gude, 2015].

Water pumping is also the major energy-consuming process in the water distribution system. The energy consumption depends on the topology of the region, the quality of the infrastructure (for example, if there is a high amount of leakage in the pipe system), as well as the distances over which water has to travel to the consumers. Water consumption itself also often consumes additional energy, mainly for heating or cooling the water to a desired temperature.

Apart from desalination, wastewater treatment is the most energy-intensive process in the water cycle. Gude [2015] states that it typically requires between 0.5 and 2 kWh of energy to treat 1 m^3 of wastewater. The energy requirements for wastewater recovery, such that water can be reused for human purposes, are in a similar range. In the United States, wastewater treatment accounts for around 3 percent of total electricity consumption [Gude, 2015]. Additionally, wastewater treatment causes carbon dioxide emissions of 45 million tons per year in the U.S., due to the degradation of organic waste.

2.3 Modelling the energy-water nexus

Several studies model the energy-water nexus with varying focus of analysis. For example, Chen and Chen [2016] apply an ecological network analysis framework for modelling the urban energy-water nexus, and apply it to a case study of Beijing, China. Ecological network analysis treats an ecosystem as a network of interconnected sectors and examines the structure and dynamics by accounting for all direct and indirect flows between different sectors. Other common approaches to assess urban systems are material flow analysis [Niza et al., 2009, Kennedy et al., 2011] and input-output analysis [Chen and Chen, 2015].

Baliban et al. [2012] develop a model for integrated heat, power, and water systems using heat engines that recover electricity from waste heat, and treatment units that process and recycle wastewater. Gabriel et al. [2016] consider the integration of industrial heat, power and water via hybrid thermal-membrane desalination. DeNooyer et al. [2016] analyse the current and future water requirements for cooling in thermal power generation in Illinois, using a geographic information systems (GIS) model.

Models of the energy-water nexus can also be found in the field of Operations Research. For instance, Santhosh et al. [2014] develop an economic dispatch (ED) model to co-optimize the dispatch of power generation and potable water treatment. They specifically allow for co-production of water and energy in a single utility, representing for example hydroelectric or thermal desalination, which can serve either the power demand, or the demand for potable water. They test their model for a hypothetical energy-water system with four power plants, three co-production plants and one water plant. Their findings suggest that the co-production of energy and water can lead to a crowding out of single product plants in either system, which could be dispatched for a lower price. Yang et al. [2014] proposed a mixed integer linear (MILP) model to determine optimal water consumption in shale gas production. Tsolas et al. [2018] use a generic graph-theoretic network approach that accounts for the interactions between energy and water flows to identify redundant subsystems and redesign the nexus for optimal resource generation and utilization.

3 Definition and potentials of (industrial) DR

We define DR as any change of the usual electricity demand pattern in response to a price signal from the electricity supplier. One possible reaction is load shedding, where the electricity use is reduced during peak hours without a change of the consumption pattern during the rest of time [Albadi and El-Saadany, 2008]. Another reaction is to shift electricity demand from peak to off-peak periods [Albadi and El-Saadany, 2008], while not reducing the overall consumption. Load shifting is particularly beneficial for processes with a certain degree of inertia or storage capabilities [Palensky and Dietrich, 2011]. On-site electricity generation increases flexibility in terms of electricity demand from the grid as well. However, we do not view this as DR according to our definition, since producing electricity on-site does not lead to a change in consumption pattern, but rather to a change in electricity supply sources.

DR can be a beneficial source of flexibility for the power system. It helps to reduce peak demand, such that the output from expensive and carbon-intensive peak units is decreased [Nolan and O'Malley, 2015]. It can potentially defer investments in generation, distribution and transmission infrastructure [Albadi and El-Saadany, 2008], because the existing infrastructure is more efficiently used. DR can also act as a reserve resource, and replace reserve capacity which would normally be provided by additional generators [O'Connell et al., 2014].

The variability in energy supply from RES creates a need for flexible demand resources in order to minimise curtailment of RES. That is why DR is seen as a promising tool to support the integration of RES into the system. In general, research finds a positive effect of DR on the energy consumption from RES and consequently on emission reduction. Finn and Fitzpatrick [2014] analyse the potential of price-based DR from two industrial consumers to increase their proportional use of wind energy by load shifting. Findings suggest that a load shedding strategy has little or no impact on wind consumption, while shifting demand from peak periods to off-peak periods improves both price performance and wind energy consumption. Müller and Möst [2018] investigate the role of DR for the system integration of RES in Germany. They show that RES curtailment can be reduced with the help of DR. However, its effectiveness for the long term integration of RES is limited by the flexibility of available DR resources.

The potential of industrial DR has been subject to several studies. Cappers et al. [2010] state that 14,800 MW of the existing DR customer base in the US comes from the industrial sector, while the residential sector provides about 6,000 MW of DR resources. Gils [2014] estimates the theoretical DR potential for Europe, including 30 different electricity consuming sectors with a load shedding or shifting potential of a minimum of one hour. Processes with short intervention times, such as cooling, air conditioning and wastewater treatment, show the biggest potential for DR. Gils [2014] finds that an average hourly load reduction of 93 GW and an average hourly load increase of 247 GW is theoretically achievable. Wang and Li [2015] conduct a survey of 43 ToU pricing schemes for industrial customers in the US. They point out that customers which do not adjust their production schedule when switching from a flat to a ToU tariff, can ultimately face higher electricity costs. Therefore, cost savings range from -72.0 to +82.6 percent, depending on the adaptability of the production schedule.

Specific characteristics of industrial customers can limit the potential for DR. The energy infrastructure (electricity meters and sensors) on site, the intertemporal interdependency of production processes and the precision in timing that some processes require [Samad and Kiliccote, 2012], can be the main limiting factors for the ability to react to a DR signal. Concerns about revealing confidential and competition-sensitive electricity

demand data can also impede the participation in DR programmes [Samad and Kiliccote, 2012].

4 DR modelling

The literature on DR modelling is extensive and a wide range of DR models have been developed so far. Comprehensive reviews on DR models have already been conducted before. For example, Boßmann and Eser [2016] analyse 117 DR models and cluster them in terms of pricing schemes, electricity systems, specific end-uses and control-strategies. They find that existing DR models are highly heterogeneous and the field lacks a body of standard models. One major insight from their analysis is that the residential sector is in the focus of many models, while industrial end-users are underrepresented. They also find that a majority of models deal with system performance, while little attention is paid to control strategies. Deng et al. [2015] also perform a short summary of DR models and categorise the existing literature in terms of the mathematical modelling approach. The most used approaches are convex optimisation, game theory and dynamic programming. Other modelling approaches include markov decision processes, stochastic programming and particle swarm optimisation. The review by Wang et al. [2017a] focuses on integrated DR in multi-energy systems. They focus on DR provision by processes in between the energy sectors of electricity, thermal energy and natural gas. It shows that research on the DR modelling of heat pumps and power-to-gas technologies is extensive. However, they point out that most studies develop a detail model of these devices, while neglecting the energy system effects.

One paper that particularly reviews scheduling models for industrial processes in order to determine operational flexibility is given by Zhang and Grossmann [2016]. Flexibility in operation is the precondition for industrial consumers to be able to participate in DR programmes. Most of those models focus on continuous processes and only some deal with batch production. They either apply a network structure with material handling constraints or base the modelling on operating modes, where the process can only operate in one of a number of predefined states. The industry processes reviewed include cryogenic air separation, aluminium and cement production, the chlor-alkali process, flour and pulp production, machining and steel production.

For an overview on the most recent literature on DR modelling, we review publications between 2001 and 2018 which develop or refer to a DR model. To explore the DR potential of wastewater treatment facilities, a sector-integrating energy system model which allows representing the wastewater treatment process in detail as well as the power system dynamics is necessary. Therefore we focus on the energy system models which analyse end-user specific DR from a system perspective and process models which analyse the DR potential of specific (industrial) consumers or applications by modelling the industrial process in detail. We also focus on system models which account for more than one energy sector or focus specifically on the DR potential of industrial consumers.

4.1 Energy system models

We found 28 publications between 2001 and 2018 which deal with an energy system model which incorporates DR. We specifically focus on publications dealing with more than one energy sector and/or industrial consumers. Most of the models are economic dispatch (ED) or unit commitment (UC) models with a cost minimisation approach. We also find some capacity planning models accounting for DR, as well as two game theoretical models. A summary is given in table 1.

ED models aim to minimise the operating cost of the whole energy system by determining the optimal power output of each generator at each point in time [Zhu, 2015]. The optimisation is subject to system constraints including the energy demand, technological constraints of generating units, availability of resources and fuels or regulatory constraints.

UC models also determine the optimal output of each generator at each time step, but additionally consider that generators can be turned on or off dynamically. That means that not necessarily all available generators in the system provide energy all the time. The decision to engage a generator in the energy supply depends on the trade-off between the costs for that generator of providing energy and the costs of switching it off. This makes the UC problem more complex than an ED, since the model is optimised over the whole optimisation period at once. Additionally, the mathematical structure of the problem changes from a linear optimisation problem in the case of ED to a mixed integer linear programme for UC due to the binary decision whether to switch generators on or off.

Model type	Publication	Focus
Unit commitment	Keane et al. [2011]	Wind penetration
	Dietrich et al. [2012]	Wind penetration
	Wang and Li [2015]	Wind penetration
	Zhong et al. [2015]	Wind penetration
	Kwag and Kim [2012]	DR constraints
	Wang et al. [2013]	Spinning reserve
	Papavasiliou and Oren [2012]	Decentralisation
	Ikedo and Ogimoto [2013]	Energy storage
	Liu and Tomsovic [2014]	Demand bidding
Economic dispatch	Behrangrad et al. [2012]	Air conditioning
	Hedegaard et al. [2012]	Heat pumps
	Papaefthymiou et al. [2012]	Heat pumps
	Lund and Kempton [2008]	Electric vehicles
	Moura and de Almeida [2010]	Multiple objectives
	Abdi et al. [2016]	Non-linear responsive loads
	Yujun et al. [2014]	Day-ahead scheduling
	Xu et al. [2017]	Wind penetration
	Tan et al. [2014]	Energy storage
	Soares et al. [2017]	Uncertainty in PV, EV, wind and market prices
Capacity planning models	Malik [2001]	
	Zeng et al. [2016]	
	Koltsaklis et al. [2015]	
	Choi and Thomas [2012]	Environmental policies
	De Jonghe et al. [2012]	Wind penetration
	Fehrenbach et al. [2014]	Residential heating
	Paulus and Borggrefe [2011]	Energy-intensive industries
Game theory	Mohsenian-Rad et al. [2010]	Autonomous DR
	Zugno et al. [2013]	Electricity retailers

Table 1: Energy system models incorporating DR

Among the reviewed ED and UC models, only one publication accounts for the physical processes within end-uses, in this case the heating of buildings: Papaefthymiou et al. [2012] couple a detailed thermal building model and an energy system model. In a first step, the thermal building model allows for the assessment of the operational restrictions of heat pumps within the building. Subsequently, the system model incorporates the building stock’s thermal behaviour as a form of energy storage in an electricity market.

A mixed-integer stochastic optimization model called PowerFys is used for modelling the day-ahead and intra-day electricity markets with an hourly resolution, with particular emphasis on wind forecast uncertainty.

Most models focus on analysing the power system, and do not account for any other energy sector. If they do, they focus on coupling electricity with heating or transport. Lund and Kempton [2008] and Hedegaard et al. [2012] use a general energy system analysis tool called EnergyPLAN. It is a deterministic input-output model and integrates the electricity, transport, industry and district heating sectors. It incorporates data on technology capacities in the system, conversion efficiencies between different energy sources, energy demands, fuel costs and CO₂ costs. The model outputs comprise energy balances, energy productions, fuel consumption, electricity imports/exports, CO₂ emissions, and costs. Lund and Kempton [2008] use the model to analyse the effect of electric vehicles and the “vehicle-to-grid” technology as energy storage within the power system on the reduction of excess wind energy. Hedegaard et al. [2012] focus on the utilisation of heat pumps and heat storage devices to integrate more wind energy into the power system.

Most studies which investigate DR within an energy system model do not specify the type of end-user providing DR, but rather incorporate a generic DR resource. Those which focus on specific end-uses analyse electric vehicles [Lund and Kempton, 2008] or heat pumps [Hedegaard et al., 2012, Papaefthymiou et al., 2012], for instance. Exclusively, the planning model of Paulus and Borggreffe [2011] focuses on energy-intensive industries: they investigate the DR potential of some important industrial processes, namely the chlor-alkali process, mechanical wood and pulp production, the aluminum electrolysis, electric arc furnace (to produce steel) and cement mills from a technical and economic perspective. For their analysis, they extend the Dispatch and Investment Model for Electricity Markets in Europe (DIME), which is a linear optimisation model that minimises total costs of the liberalised European electricity market. It provides long-term forecasts for investment decisions and the optimised economic dispatch for spot- and reserve markets. Within this framework, Paulus and Borggreffe [2011] model DR resources with a potential for load shedding similarly to power plants and processes with the potential for load shifting in the style of energy storage units. Technical restrictions which ensure a minimal disruption of the production process and cost parameters define the extent to which the DR resources are developed and exploited in the system. While the limiting factor for load shedding is the respective opportunity cost, load shifting is characterised by lower variable costs and is mostly limited by the storage capacity of the DR resource. The findings of Paulus and Borggreffe [2011] suggest that DR from the investigated industrial processes could technically provide up to 50 percent of capacity reserves for the balancing market in 2020. However, they qualify this figure by pointing out that load shedding processes are generally not suitable to provide balancing power in real-time, due to the high opportunity costs of lost loads in the production process. Therefore, they see more DR potential for load shifting processes within the industry sector.

Another planning model which investigates a specific DR resource in an integrated energy system model is Fehrenbach et al. [2014]. They use the TIMES (The Integrated MARKAL-EFOM System) model, which is a widely used energy system optimisation tool and combines a technical engineering and an economic perspective. It uses linear-programming to produce a least-cost solution for the energy system over medium to long-term time horizons [Loulou et al., 2005]. Fehrenbach et al. [2014] use TIMES for modelling the electricity and residential heat supply in Germany and to determine capacity developments and dispatch of electricity and residential heat generation technologies until 2050. Other capacity planning models such as De Jonghe et al. [2012], Choi and Thomas [2012] and Malik [2001] take a more generalised approach and do not specify the end-user which

is providing DR.

We also reviewed two DR models in the realm of game theory. These models do not have a single objective function which is optimised for the whole energy system, but acknowledge the presence of multiple players with individual objectives within the system. The outcome of the optimisation depends on the structure of the game, e.g. the order in which players choose their strategies and which information is available to them. Therefore, these models can account for strategic behaviour among players, as well as for information asymmetries. One of those models is introduced by Zugno et al. [2013]. They model the relationship between electricity retailers and consumers as a Stackelberg game with a dynamic pricing scheme. They find that dynamic pricing is more effective in achieving load-shifting than fixed and time-of-use pricing. Meanwhile, Mohsenian-Rad et al. [2010] focus on the interaction between energy users in a distributed energy supply system, rather than on the relation between energy users and energy utilities.

4.2 Process models

In contrast to energy system models, process models (or load models) focus on a process, device or application of a particular end user. In those models, DR activity is triggered by an exogenous price signal from the power market. The objective of those models is to find an optimal process schedule given the technical constraints of the process and cost parameters. Several process models deal with the DR potential from industrial processes. The traditional way of modelling an industrial process involves the detailed description of the system's performance, e.g. its thermodynamics and kinetics [Mitra et al., 2012]. This requires the formulation of heat and mass balances for each process module. However, following this approach can make a model extremely complex due to its non-linearity and its size and therefore it is hard to solve for longer time horizons. Instead, the models presented in the following focus on the electricity demand of the process and abstract from the physical details. Table 3 gives an overview of all reviewed process models dealing with DR, grouped into three different process types: thermal appliances, transport (electric vehicles) and industrial processes. The following section will focus on industrial process models which analyse the DR potential of the process.

Process type	Publication	End-use	Model description
Thermal appliances	Fitzgerald et al. [2012]	electric water heaters	Control algorithms with different objectives
	Hong et al. [2012]	heat pumps	Discrete demand side control (DDSC) algorithm
	Stadler et al. [2009]	Cooling devices	Thermal control model
	Hovgaard et al. [2012]	Refrigerators	Model predictive control
	Moreau [2011]	Domestic water heaters	Control algorithm
	Parkinson et al. [2011]	Heat pumps	Network control strategy
	Zehir and Bagriyanik [2012]	Refrigerators	Thermal control model
	Zhang et al. [2012a]	Residential thermostatical loads	Aggregated physical models
	Knudsen and Petersen [2016]	Space heating	Model predictive control
	Hu et al. [2017]	Residential air conditioning	Grey-box room thermal model
	Palensky and Dietrich [2011]	Heating in buildings	Simplified process models
	Bianchini et al. [2016]	Heating in buildings	Model predictive control
	Lauro et al. [2015]	Heating in buildings	Model predictive control
Multiple appliances	Hu and Xiao [2018]	Inverter air conditioners	Genetic algorithm
	Paull et al. [2010]	Domestic water heaters	Predictive thermal model
	Goddard et al. [2014]	Commercial HVAC	open-loop control algorithm, based on statistical models
	Shao et al. [2012]	Domestic space cooling and heating, water heater, clothes dryer and electric vehicle	Aggregated physical models
	Abdulaal et al. [2017]	Industrial loads: multi-stage chiller system, EV charging, and EV discharging for building's demand support (V2B)	Quadratic, stochastic, and evolutionary programming with multi-objective optimization and continuous simulation

Table 2: Process models incorporating DR

Process type	Publication	End-use	Model description
Transport	Ahn et al. [2011]	Electric vehicles	Decentralized charging control algorithm, minimising electricity cost and emissions
Industrial processes	Ashok [2006]	Steel plants	Integer programming
	Ding and Hong [2013]	Steel plant	State task network (STN)
	Ding et al. [2014]	Industrial consumers	STN and MILP
	Reka and Ramesh [2016]	Refinery industrial plant	Resource-task network processing model
	Middelberg et al. [2009]	Colliery process	Binary integer programming
	Wang et al. [2017b]	Chlor-alkali plant	Deterministic MILP
	Mitra et al. [2012]	Air-separation process	
	Rodríguez-García et al. [2016]	Industrial consumers	
	Sianaki et al. [2018]	Industrial consumers	Linear programming
	Zhang et al. [2016]	Industrial loads	Model predictive control
	Hindi et al. [2011]	Industrial process	Model predictive control
	Helin et al. [2017]	Pulp and paper mill	MILP
	Mohagheghi and Raji [2014]	Vehicle cockpit manufacturing	Fuzzy logic

Table 3: Process models incorporating DR

Ashok [2006] develops a load model for small steel plants in India under a time-of-use (TOU) tariff regime. The model is coupled with an optimisation formulation utilising integer programming for minimising the total electricity cost satisfying production, process flow and storage constraints. The author claims that it can also be applied to other batch-type processes. Middelberg et al. [2009] explore optimal control strategies of the colliery process and conduct a case study for a colliery in South Africa. The control strategy emerges from minimising the total electricity costs of the process, with a binary decision variable for every module of the process. They discretise the time horizon of the optimisation window, which turns the scheduling problem into an integer programme.

Mitra et al. [2012] develop a discrete-time, deterministic mixed integer linear model for scheduling power-intensive continuous processes. The objective function is composed of the production cost, inventory cost and transition cost of the process. This is minimised for every hour with an emphasis on the operational transitions, which arise from switching the operating modes of the process modules. They show that certain logic constraints limit the flexibility in control severely. Given hourly electricity prices, they conduct a case study on air-separation plants and cement plants and demonstrate that their model yields practical schedules, while minimising the number of changeovers. Ding and Hong [2013] provide a process model for industrial consumers which can incorporate on-site electricity generation, e.g. by solar panels, wind turbines or waste heat recovery, and energy storage. The mixed integer linear model is based on a state task network (STN) approach, which divides tasks into non-schedulable and schedulable. Hence, only schedulable tasks can be used to provide DR, because they can be run in multiple operating modes, with varying production rates and electricity demand. This structure yields a relatively straight-forward framework to model any industrial process with a focus on

DR. Ding and Hong [2013] demonstrate the model structure with the help of a case study for steel manufacturing facilities. However, they do not provide any results on the scope of DR in this case study nor specify the required DR algorithms and strategies according to which the tasks should be scheduled.

In another study, Ding et al. [2014] apply the same model to the industrial oxygenating generation, which is part of many industrial processes like steel and glass manufacturing or wastewater treatment. DR decisions are based on day-ahead hourly electricity prices. The optimisation yields a process schedule where energy demand is shifted from peak to off-peak periods, which results in a reduction of total energy costs.

Reka and Ramesh [2016] use a similar approach called resource-task network processing modelling. They also distinguish between schedulable and non-schedulable tasks within the process, but pay special attention to the resources consumed in every task. They use stochastic optimisation with discrete time steps. The proposed DR algorithm aims to minimise the total process costs. The model is tested with a case study for an oil refinery with on-site electricity co-generation facilities. The most energy-intensive refinery sub-processes are desalination, hydro-treatment and crude oil distillation. Findings suggest that employing DR strategies for schedulable tasks yields a shift in energy demand from peak to non-peak periods.

Rodríguez-García et al. [2016] introduce a model for industrial customers to perform a cost-benefit analysis of the implementation of DR strategies. In contrast to most other (prescriptive) models that we found, this is a dynamic simulation model, which relies on the identification of typical load curves by an energy audit. The decision criterion for whether a process should participate in DR is the difference between the net amount of money that the industrial customer receives due to the participation in the reserve energy market, and the expected benefit for the customer. The authors make the model available to industrial customers as an online tool and show an application for a German paper factory. Although they claim that the model has been validated in four real industrial sites from different parts of Europe, it does not sufficiently account for the interdependence of sub-processes and therefore yields a skewed picture of the economic DR potential.

Zhang et al. [2016] recognise that many industrial processes can technically provide fast DR, but most of them can only vary electricity demand discretely in the form of certain MWs at a time. However, providing fast DR can require a more granular change in power. In order to overcome this, the authors propose a process model which incorporates on-site energy storage. As a case study, the authors choose mills in a cement plant, which can be switched on and off very rapidly. A model predictive controller (MPC) coordinates a large discrete power change provided by the industrial process and a small continuous power change provided by the energy storage, such that the total power change accurately follows the DR signal. The MPC approach combines a stochastic model for inputs, e.g. a price signal, with a short-term optimisation of the connected processes. It is a common approach that can be found in many industrial process models that investigate DR potentials (see table 3).

In the model of Zhang et al. [2016], DR is achieved by incorporating the satisfaction of the DR signal along with the number of switching actions in the objective function of the optimisation model. The results demonstrate that the MPC regulates both the industrial loads and the energy storage effectively to provide fast and high-quality DR. Wang et al. [2017b] conduct a case study on DR from a grid-connected chlor-alkali plant with an integrated on-site energy recovery system. They develop a communication and incentive scheme that incorporates day-ahead process scheduling according to the electric-

ity contract, as well as real-time DR. Total operating and environmental costs through producing, purchasing and selling electricity are minimised while meeting production requirements. The results show that the average electricity costs are lowest with an energy contract based on demand responsive behaviour.

5 The WWTP process

5.1 WWTP modelling

Gernaey et al. [2004] review state of the art process modelling approaches for activated sludge-type WWTPs. Activated sludge is the most common technology used in WWTPs with secondary treatment, i.e the process includes the removal of biodegradable organic matter and suspended solids [Tchobanoglous et al., 2003]. The core process includes the injection of air into the reactor tanks, which facilitates the growth and respiration of micro-organisms that are able to break down organic and nitrogenous matter in the wastewater [Aghajanzadeh et al., 2015]. Figure 3 depicts the basic activated sludge process. It consists of a primary settling tank, an aerated tank in which the micro-organisms are kept in suspension, a sedimentation tank to separate liquids and solids by gravitation, and a recycle system which returns sludge back into the aerated tank [Tchobanoglous et al., 2003].

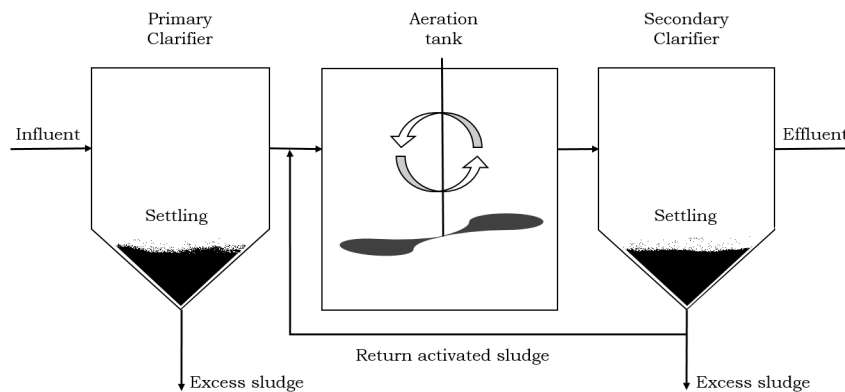


Figure 3: Basic activated sludge process

The reference model, primarily used to model municipal activated sludge plants, is the Activated Sludge Model 1 (ASM1) developed by Henze et al. [1987]. It is a white-box model which describes the biochemical processes within the aerated tank by eight process equations and 13 state variables [Jeppson, 1996]. White-box models, or deterministic models, consist of a set of differential equations that are based on fundamental physical principles. Other important WWTP applications like the prediction of the influent load or the estimation of biomass activity and effluent quality use black-box or stochastic grey-box approaches [Gernaey et al., 2004]. White-box models can also be complemented by Artificial intelligence (AI) methodologies, for example in the form of supervisory control systems [Gernaey et al., 2004].

While white-box models can only evaluate scenarios based on existing process knowledge about the WWTP, AI methods can also extrapolate knowledge from experience, in order to enhance WWTP control [Gernaey et al., 2004]. Other data-driven approaches are used to model specific subprocesses within the WWTP. For example, Asadi et al. [2017] use a data-mining approach based on input-output data to optimise the aeration process of a WWTP in Detroit, MI. The authors use a combination of the multi-adaptive regression spline (MARS), Artificial Neural Networks (ANN), Random Forest (RF) and K-nearest neighbor (k-NN) to construct the aeration model. The approach is data-intensive, as the training set for the algorithms contains 4368 data points and the testing set contains

2544 data points. The model minimises the dissolved oxygen (DO) concentration in the wastewater as a proxy for energy consumption for aeration. However, the ASM1 is often still the state of the art activated sludge model, with many expansions and modifications.

The ASM3 model, for instance, proposed by Gujer et al. [1999], corrects for a number of shortcomings of the ASM1 model, like inflexibility in settings for the external temperature, pH values, water toxicity, wastewater composition and the kinetics of bio degradation. Both ASM1 and ASM3 are used for WWTP design and for determining optimal process control strategies.

Based on these models and benchmark data, commercial WWTP simulators are available to model the whole WWTP process or specific sub-processes. These WWTP simulators often contain a preinstalled library of WWTP models. The process can easily be configured by connecting predefined unit blocks and modifying the model parameters. Examples of commercial modelling software are AQUASIM, BioWin WEST, EFOR, GPS-X, ICS, SIMBA#water, STOAT and Sumo. With the help of these simulation platforms and based on the ASM model family, a variety of WWTP models have been developed. They differ in plant layout and treatment technology and are often build to fit the characteristics of a real WWTP.

5.2 Flexibility potential within the wastewater treatment process

There is a slight tendency towards load shedding strategies across the reviewed case studies that explore the flexibility potential for WWTPs. However, the potential for load shifting is also addressed in some publications. The opportunities for flexible operation are investigated for the aeration in the activated sludge and for wastewater pumps at several stages of the treatment process in conjunction with the use of overcapacity in the tanks [Schäfer et al., 2017, Aghajanzadeh et al., 2015]. Anaerobic sludge digestion, which is a part of many modern WWTPs, also allows for flexible operation. Additionally, the process generates biogas, mainly CO₂ and methane, which can be used to produce electricity on-site.

A typical domestic wastewater treatment plant with sludge treatment consumes approximately 0.6 kWh of energy per m³ of wastewater treated [Gude, 2015]. Most electric energy is required for the aeration in the activated sludge process and the wastewater pumping. Figure 4 shows the shares of the electricity consumption in the influent pumping and the aeration process from the total energy consumption of plants with a conventional activated sludge (CAS) system, as monitored in different case studies [Foladori et al., 2015, Smith, 1973, Malcolm Pirnie, Inc., 2005, Electric Power Research Institute, 2002, SAIC, 2006, Panepinto et al., 2016, Longo et al., 2016]. It can be seen that the aeration in the activated sludge process consumes the highest share of electricity, ranging between 10.2 and 71 percent of total electricity consumption. Depending on the topology of the plant, the inflow pumps consume up to 15 percent.

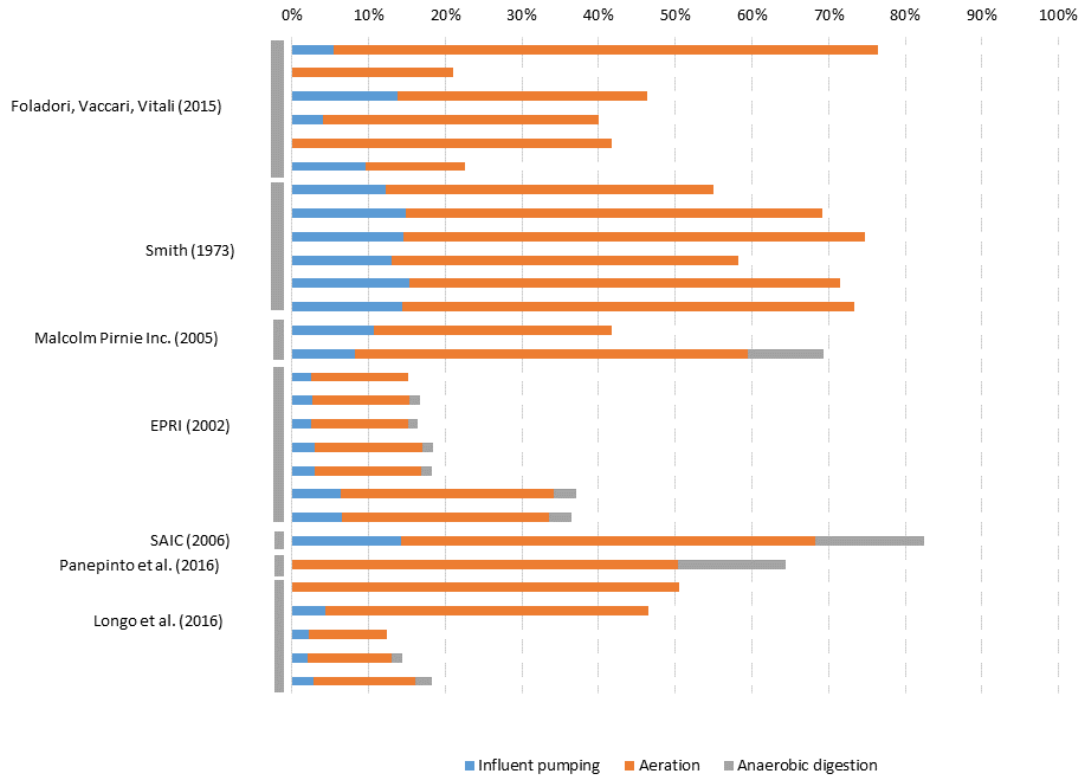


Figure 4: Share of total energy consumption across case studies

Therefore, many studies have performed energy audits (see some examples in table 4), looking into the possibilities to improve energy efficiency [Foladori et al., 2015, Guerrini et al., 2017] and to save energy in pumping and aeration [Awe et al., 2016, Panepinto et al., 2016]. Fewer studies explore the technical potential for flexibility and assess the economic potential of changing their operating state according to energy prices.

Data type	Energy audits	Country	Number of plants
Total energy consumption (and biogas production) (and other cost factors)	Silva and Rosa [2015]	Portugal	17
	Bodik and Kubaska [2013]	Slovakia	51
	Hernández-Sancho et al. [2011]	Spain	177
Total energy costs	Guerrini et al. [2017]	Italy	127
	Póvoa et al. [2017]	Portugal	1
Energy consumption of all subprocesses	Foladori et al. [2015]	Italy	5
	Awe et al. [2016]	Ireland	1
	Panepinto et al. [2016]	Italy	1
	Wett et al. [2007]	Austria	1
	Schäfer et al. [2017]	Germany	1

Table 4: Exemplary published energy audits of WWTPs

The flexibility options reviewed are the sludge processing, the aeration process, the wastewater pumping and the use of built-in redundancy. Since the aeration and the pumping consume significant amounts of electricity, they can be classified as flexibility options that can be used to provide DR. In contrast, one can argue that the flexibility

provided by biogas production cannot be classified as a DR action, since the flexibility does not arise from load shedding or load shifting of an electricity-consuming process, but rather from the production and self-consumption of electricity. However, the ability to produce electricity on-site affects the energy consumption from the grid and consequently the DR provision. Therefore, the flexibility options within the sludge processing are reviewed first, followed by the flexibility potential of the aeration process and the pumping. We also explain how the use of built-in redundancy affects the flexibility potential of the pumps.

5.2.1 Sludge processing

Sewage sludge is a by-product of the wastewater treatment process. It refers to the solid part of the wastewater that settles down in the tanks and is generally disposed to landfill or used for land applications. Prior to disposal, the sludge needs to be dried in several steps in order to reduce its volume. This sludge treatment can account for about 30 percent of a plants operating costs [Shen et al., 2015]. After thickening the sludge, it enters the anaerobic digestion system, normally consisting of a reactor filled with liquid sludge, and a sealed gas headspace Batstone et al. [2002]. The biochemical and physico-chemical reactions within the sludge release biogas to the headspace, which can be extracted into storage tanks for further utilisation. Afterwards, the remaining sludge is dewatered, typically in a centrifuge, for final disposal. Figure 5 depicts the sludge treatment process.

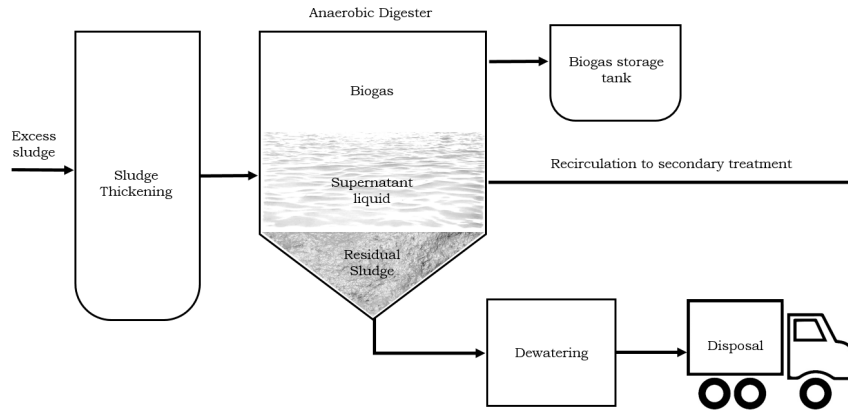


Figure 5: Sludge treatment process

Due to the fact that the sludge is rich in nutrients and energy, it has a variety of potential applications, including fertilizer substitution or renewable energy production [Shen et al., 2015]. A major part of the energy content of the sludge is captured in methane [Wett et al., 2007]. In the form of biogas, this energy can be transformed into electrical (and thermal) energy by a combined heat and power (CHP) plant or used as a transport fuel. The electric energy produced by an on-site CHP can either be used to drive the aeration system or heat the sludge digesters [Wett et al., 2007]. Shen et al. [2015] claim that biogas recovery from sewage sludge has the potential to make a WWTP energy self-sufficient and even turn it into a net energy producer.

Seier and Schebek [2017] develop a WWTP process optimisation model that focuses on the flexibility potential from WWTPs in Germany. They assess the effects of load shifting by WWTPs on residual load smoothing. The residual load refers to the total power consumption minus the feed-in of renewable energies. The load shifting potential arises solely from a biogas storage option, which can be used to generate electricity on-site in a CHP plant. Their findings suggest that German WWTPs, which are using biogas for electricity generation, have a potential to integrate 120 MW of surplus electricity. Seier and Schebek [2017] use a separate merit order simulation to model wholesale electricity

prices, which are then fed into the WWTP optimisation.

Schäfer et al. [2017] finds the greatest flexibility potential within a WWTP in Germany in the operation of a CHP unit fed by biogas from the anaerobic digestion. Based on this, Schmitt et al. [2017] calculate a total flexibility potential for WWTPs in Germany of 2,057 MWh/day of additionally available load and 2,391 MWh/day of curtailable load for the whole treatment process. The majority of this flexibility is based on the availability of CHP for on-site electricity generation. Gude [2015] estimates that biogas produced from anaerobic digestion can cover up to 50 percent of the total energy needs for sludge treatment and that WWTPs can even become net energy producers if energy recovery rates from biogas increase.

5.2.2 The aeration process

The aeration process is an essential part of a CAS system, which is the most common treatment technology among WWTPs with secondary treatment. The injection of air into the reactor tanks supports the growth of microorganisms that break down the organic and nitrogenous matter in the wastewater [Aghajanzadeh et al., 2015]. The two main methods of aerating wastewater are mechanical surface aeration, where the water is aerated by agitation of the water surface, and the use of submerged diffusers to inject air or pure oxygen directly into the wastewater [Bolles, 2006]. In the activated sludge process, diffused aeration systems are commonly used. They typically consist of blowers, air pipes and diffusers [Brandt et al., 2006]. The size and number of blowers and diffusers is determined by the biological oxygen demand (BOD) of the wastewater and by the efficiency of the equipment [Aghajanzadeh et al., 2015].

In CAS systems, the aeration within the aerated tank is a continuous process in order to provide a stable environment for the bacteria which perform the organic decomposition. Other treatment technologies, e.g. the sequencing batch reactor (SBR), employ a strategy of intermittent aeration in order to create a cycle of anoxic and aerobic conditions within the tank [Tchobanoglous et al., 2003].

This illustrates that the required energy for aeration highly depends on the type of treatment technology. Additionally, factors such as the population of aerobic bacteria, the pollutant loading of the wastewater, the standards for effluent quality, and the size and age of the treatment plant play an important role [Awe et al., 2016]. Seasonal variations of inflow patterns and weather conditions also determine the aeration requirements. On the one hand, the overall wastewater inflow is lower during dry months [Lekov, 2009], which reduces the aeration requirement e.g. during summer. On the other hand, it has to be taken into account that the DO concentration is a function of temperature [Tchobanoglous et al., 2003]. With higher temperatures, the oxygen demand for biochemical reactions increases [Aghajanzadeh et al., 2015], which means that maintaining DO levels requires more extensive aeration during summer months [Tchobanoglous et al., 2003]. Determining the optimal operating schedule of the aeration process requires the consideration of all these factors.

Several case studies find that shutting down the aeration in peak periods is possible for a limited amount of time without a significant change in effluent quality. Schäfer et al. [2017] conduct a case study on a German WWTP and find that the aeration can be switched off for 60 minutes without a significant decline in effluent quality, with a maximum effective power flexibility of 98.6 kW. Müller and Möst [2018] find that the aeration can be turned down for 30 minutes at maximum at day-time and up to 120 minutes during night-time. Nowak et al. [2015] come to a similar result, turning off the aeration for a period of 60 to 120 minutes without breaching the effluent standards. In contrast, Berger

et al. [2013] and Kollmann et al. [2013] evaluate a possible switch-off duration of only 15 minutes. In another case study of a California WWTP by Thompson et al. [2010], switching off the aeration for 120 minutes negatively affected the effluent turbidity. This shows that the technical flexibility of plant equipment can vary significantly.

Thompson and McKane [2008] propose the idea of excessive aeration during off-peak periods to extend the switching-off time during peak periods. This is based on the idea that the DO concentration within the water can be increased by over-aerating the water. Ideally, this could extend the phase in which the DO concentration is decreasing when the aeration is off, down to a critical level when the aeration has to be switched back on. To our knowledge, there have not yet been any case studies of WWTPs to test for its feasibility. Neither have there been any attempts to model over-aeration to investigate its DR potential. However, Brdjanovic et al. [1998] demonstrates the negative impact of excessive aeration on the process efficiency, namely the biological removal of phosphorus. The fact that only a limited amount oxygen can be dissolved in water [Tchobanoglous et al., 2003] might restrain the flexibility potential even further.

5.2.3 Wastewater pumping

Wastewater pumping is often the second most energy-intensive process in a WWTP after the aeration [Awe et al., 2016]. Pumping is necessary in the form of inlet pumps, because topographic conditions often prevent the wastewater from flowing into the WWTP naturally. Even in the case of favourable topography, inlet pumps are often in place due to the texture of the sewage, that results in an innately slow flow rate. Additionally, sludge recycle pumps are used to recycle a part of the sludge from the secondary clarifier back into the aerated tank (see figure 1). This is necessary to maintain the bacteria concentration within the aerated tank. Both processes have been subject to research to explore their potential for load shedding and load shifting.

In the case study of Schäfer et al. [2017], it was possible to switch off the sludge recycle pumps for 120 minutes without a negative effect on the effluent quality, providing a maximum of 23.6 kW of effective power for flexibility. According to a case study in California from Olsen et al. [2012], lift pumps and external pump stations show potential for load shifting, because of their low ramp rates.

Many studies investigate how to operate pumps in WWTPs with minimum energy consumption [Torregrossa et al., 2017, Zhang et al., 2012b, Chang et al., 2012, Olszewski, 2016]. However, there is not yet much published research on the potential for load shedding or load shifting of inlet or recycle pumps. An important condition for pausing wastewater pumping in peak periods is that wastewater can be withheld in the system, either in tanks or in the pipes. Many WWTPs have built-in redundancy on-site, which can potentially be used in order to operate pumps intermittently.

5.2.4 Using built-in redundancy

Particularly small-scale WWTP often have redundancy on-site, in the form of oversized or additional tanks or overcapacity in the sewers. WWTPs can extend the retention time of untreated, partially treated or treated wastewater during peak periods and process or release it later during off-peak hours [Aghajanzadeh et al., 2015], if site conditions allows for longer wastewater retention. In the energy audit performed by Foladori et al. [2015] (see figure 1), the design capacity of all WWTPs exceeds the capacity which is actually used for treatment. Schäfer et al. [2017] find in their energy audit that small-scale WWTPs have more unused capacity than larger WWTPs, due to oversized equipment. Furthermore, large WWTPs are often already operated at optimised level, while small WWTPs often

operate below design capacity. This is often due to a lack of adequate monitoring devices in smaller plants.

The study by Olsen et al. [2012] finds potential for flexibility in pumping due to overcapacity in the San Francisco sewer system and the WWTP. Findings suggest that lift pump could be curtailed for several days. However, the authors emphasise that the redundancy serves the purpose to account for the risk of heavy rain fall events. Using it for the provision of DR means that the safety margin given by redundancy decreases. An unanticipated exposure to a sudden rainfall event when sewers and tanks are already heavily loaded increases the risk of over-stressing the system and discharging untreated wastewater. Therefore, they conclude that the use of redundancy for DR must be evaluated carefully based on high-quality weather forecasts.

6 Discussion

Wastewater treatment is an electricity-intensive process and a coordinated DR programme for WWTPs could have a significant impact on the power system. The participation in DR programmes is potentially beneficial for the plant operators in order to achieve savings in electricity costs by making use of time-varying electricity rates. The implementation of the options presented in section 4.2 (excluding the installation of a CHP plant for on-site electricity generation) do not require significant investments in additional technology which could hamper the net cost savings. Wastewater flows follow a diurnal pattern that coincides with electricity demand patterns, with one peak in the late morning and another one during the early evening between 7 and 9 pm [Thompson and McKane, 2008]. If wastewater treatment is carried out according to this pattern, the electricity demand of the WWTP is high when overall system demand is high.

Time-varying pricing schemes, like time-of-use (TOU) tariffs or real-time pricing (RTP), offer lower electricity rates during off-peak hours and penalise electricity consumption during peak hours with higher rates. A TOU pricing scheme consists of different tariff periods throughout the day, for example peak and off-peak periods, with a higher charge during peak periods [Samad and Kiliccote, 2012]. The time periods and tariffs are fixed upon conclusion of the electricity contract. Meanwhile, prices can change more often, mostly hourly, during a day within the RTP scheme and the tariff schedule is announced one day in advance [Samad and Kiliccote, 2012]. If WWTP operators decide to participate in a time-varying pricing scheme, a shift of treatment from peak to off-peak periods, for example from evening to night times, can yield electricity expenditure savings. The scope of potential savings depends on the degree of shiftable load. For example, Aghajanzadeh et al. [2015] estimate that the participation in DR programmes can provide energy cost savings up to 15 percent by shifting loads from peak to off-peak periods.

One challenge for the implementation of DR programmes at WWTPs is the lack of adequate monitoring and control equipment. Small-scale WWTPs in particular often do not have a metering and control system in place that allows for precise DR interventions. The expensive installation of meters and controls and ideally an automated control system can prevent plant operators from becoming DR providers. Furthermore, not breaching the environmental standards for the effluent quality is the top priority within a WWTP. That means that a deviation from the usual operating schedule can only be considered, if the risk of discharging water of insufficient quality is not increased.

The use of biogas for energy recovery also bears some challenges. The energetic value of biogas is determined by its CH₄ content. Since biogas has a methane content of about 55-65 percent and a CO₂ content of 30-40 percent, its energetic value is comparably low

[Appels et al., 2008]. Additionally, impurities have to be removed before biogas can be used in a CHP. That means that significant capital and maintenance costs are connected with the implementation of an on-site electricity generation system. Injection of biogas into the gas grid is possible, but only after upgrading the biogas (mainly removing CO₂) to fulfil the gas standards of the respective grid. Therefore, an enhancement system including carbon dioxide removal needs to be implemented before biogas can be sold to the gas grid, causing further capital investments.

The quantification of the potential of DR from WWTP is essential to evaluate its value added for the power system and market. The case study by Schmitt et al. [2017] indicates that DR provision by WWTPs supports the integration of more RES into the power system. Harnessing the flexibility provided by the WWTP, the share of curtailed wind energy was reduced by 92 percent. The findings of Seier and Schebek [2017] suggest a total potential of German WWTPs to integrate 120 MW of surplus electricity. However, these findings are technology- and country-specific and cannot simply be applied to other energy systems.

The evaluation of DR potential and benefits, not only in the wastewater treatment sector, is concentrated on monetary benefits, the integration of RES and CO₂ emission abatement. However, the analysis of the energy-water nexus should focus on the sustainability of the whole system. That means that the environmental effects like the emission of other pollutants and externalities that affect land use or food production should be included in the assessment of any environmental policy, and in this case, of applying a DR scheme for WWTPs.

A combined system-process model for DR from WWTP

The literature review shows that most power system models take on the form of ED or UC models. On the one hand, ED and UC models are valuable tools for studying the system effects of DR. DR influences the energy demand in the system and ideally changes the daily load profile. This can improve the utilisation of renewable energy sources, which can be analysed by means of an ED or UC model. It can also be used for quantifying the economic cost and savings of DR. Other aspects depend on the level of detail in the model. Some models incorporate the level of emissions caused by fuel use, such that environmental effects of DR are also in the scope of analysis. In addition, stochastic unit commitment can be used for representing the uncertainties related to renewable energy generation [Papavasiliou and Oren, 2012] and studying their effect on the participation in DR programmes.

The underlying assumption of all these DR models is that the system operator is capable of centrally co-optimising the dispatch of demand-side resources and generators [Papavasiliou and Oren, 2012]. In practice, however, the system operator does not have full control over the system down to the retail level [Papavasiliou and Oren, 2012]. As a result, the outcome of the ED and UC model provides a good benchmark for the potential benefits of demand flexibility, but strategic behaviour of system participants most likely yields a different system outcome in reality. This has to be kept in mind when interpreting the results from ED and UC models.

On the other hand, understanding the DR potential of a specific industrial process requires a detailed process model which takes into account minimal production disruptions and production costs. These models often consider energy price signals to be exogenous. Following this approach, industrial consumers are assumed to be price takers which do not have any influence on the market through changing the energy demand profile. However, a coordinated DR signal across multiple big industrial consumers is likely to influence

overall system demand and prices. These effects of DR on the energy system cannot be studied within the framework of a DR process model like the ones presented here. An integrated energy system should ideally incorporate both the relevant details of a process model and the power system to capture the potential for DR from a system perspective.

This literature review has shown that there is not yet a model which combines these two important aspects to perform a meaningful analysis of the DR potential from WWTPs. The reason that most DR system models abstract from the physical processes within end-use applications lies in the non-linearity that characterises many of them. Standard ED and UC models are linear or mixed integer linear programmes, which cannot handle non-linearity in constraints. The wastewater treatment process in particular is characterised by complex biological and chemical reactions with a non-linear nature. The standard WWTP models, like the ASM1 model, capture these reactions well. However, these models are mainly used for process and design simulations and integrating them into a linear optimisation framework is challenging. The constraints which determine the biological and chemical reactions within the WWTP would have to be simplified and linearised to find a balance between accuracy and computational cost. This has not yet been attempted for any WWTP model. It is also striking that none of the reviewed DR models explores the energy-water nexus. Coupling energy sectors, and especially the electricity and water sector, within an energy system framework is not yet in the focus of DR research.

There is no study that investigates the DR potential from WWTPs in an integrated energy system so far. Although studies such as Seier and Schebek [2017] assess the DR potential from WWTPs, they do not take on a power system perspective, but rather perform a cost minimisation from the plant operator’s perspective, with an exogenous electricity price signal. They also assume biogas storage and use for on-site electricity production as the only source of flexibility. In order to analyse all of the flexibility options summarised in this paper comparatively, an integrated energy-water system model of the wastewater treatment process and the power system is required. To our knowledge, such a model does not exist to date.

Our future contribution will be to identify the DR potential from WWTP not only for the plant operator, but also for the power system. This will be achieved by an integrated energy system approach, which couples the traditional MILP approach for power systems modelling with a simplified and linearised WWTP model. Within this framework, we can assess the DR potential of different electricity consumers within the plants (e.g. pumps or blowers) individually and combined, as well as take into account the variability of inflow rates due to heavy rain falls.

7 Conclusion

DR models can be grouped into two categories: energy (or power) system models, which take on a system perspective of the optimal utilisation of DR, and process scheduling models, which analyse the optimal DR strategies for a particular end-user. The review has shown that most energy system models which analyse DR focus on the power system, and do not account for any other energy sector. If they do, they focus on coupling electricity and heating or transport. Those models often do not specify the DR resource in place, but rather assume a generic unit which provides DR. Meanwhile, process scheduling models go into greater detail, but assume price signals from the power system to be exogenous.

However, significantly large DR resources cannot be viewed as mere price takers. An increase in DR in a system can be interpreted as an increase in demand elasticity. With a more elastic energy demand, price changes can be induced by either the supply or the demand side. This endogeneity of prices is not yet captured in process models which deal with DR. With respect to the size of the wastewater treatment sector and its significant electricity demand, we believe that this endogeneity has to be taken into account in order to assess the DR potential of the wastewater treatment sector.

Models which combine a detailed process model with a wider energy systems model are limited and mostly deal with district heating in buildings. Although there are also models which analyse the energy-water nexus, none of the reviewed DR models explores the energy-water nexus to date.

Furthermore, this review has revealed that the potential for WWTPs to provide demand flexibility to the power system is not yet widely studied. Several case studies explore the operational flexibility of different energy consuming processes within individual plants. These studies show that there is potential for load shifting for several processes within a WWTP and thus for the participation in DR. However, wastewater treatment process-related constraints based on these findings have to be applied to a wider energy system model in order to move from results which hold true for individual plants to conclusions which apply more generally.

The findings of the literature indicate that DR from WWTPs provides potential benefits to both the power system and the WWTP operators, but certain challenges have to be overcome to facilitate the participation of WWTPs in DR programmes. One challenge is the quantification of the system-wide potential and the evaluation of economic and environmental effects. However, there is a lack of assessment of these effects on both WWTP operators and the power system. In order to tackle this, there is a need for a suitable integrated energy system model that captures the characteristics of the wastewater treatment process and its interconnection to the power system.

Future research will deal with the development of such an integrated energy-water model which can account for the wastewater treatment operation and the operation of the power system simultaneously.

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